

1 **A comparative life cycle assessment of asphalt mixtures for railway sub-ballast containing**
2 **alternative materials**

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3

4 **ABSTRACT**

5 Bituminous sub-ballast in railway track-bed can mitigate the variation of the moisture content in the
6 subgrade and reduce vertical stiffness variations of the track leading to a more durable infrastructure.
7 Nevertheless, durability is only one of the aspects that affects the sustainability of an infrastructure.
8 Other relevant aspects are related to the environmental and economic issues. This research work joins
9 the worldwide effort towards a paradigm shift in civil engineering devoted to assess the sustainability
10 of infrastructures at the design stage. With this in mind, in this study different alternative bituminous
11 sub-ballast mixtures containing recycled materials, namely crumb rubber (CR) and reclaimed asphalt
12 pavements (RAP) were compared by means of the results of a Life-Cycle Assessment (LCA). In
13 comparison with a traditional bituminous sub-ballast the Crumb Rubber Modified (CRM) mixtures
14 showed higher impacts due to the treatment of the rubber as well as the higher amount of bitumen
15 employed in the mixture. In turn, when RAP is used, the LCA results report an improvement of all
16 the indicators considered. The reduction of the impacts is even higher when full blending between
17 the aged and the virgin binder is assumed because it allows reducing the amount of virgin bitumen
18 employed. The results are intended to be used by engineering experts and practitioners to make more
19 assertive judgments on the advantages and disadvantages associated with the use of emerging and
20 commonly called sustainable strategies and practices for railway track-bed.

21

22 **Keywords:** Bituminous mixtures; crumb rubber; reclaimed asphalt pavements; life cycle assessment;
23 environmental sustainability

24

1. Introduction

Railway transport is one of the transport modes responsible for the lowest CO₂ emissions and energy consumption when operational components, such as running vehicles, are considered. However, during the construction and maintenance operations (non-operational components) the CO₂ emission and energy consumption are considerably high comparatively to other transport modes (Chester and Horvarth, 2009; Schwarz, 2009). This gap between energy consumption and GHG emissions related to operational and non-operational components underline the need for further research efforts dedicated to the improvement of the best practices of construction and maintenance of railway infrastructures, in order to minimize their negative effects on the society and environment. Railway track-bed is typically composed of different layers, namely ballast, sub-ballast and subgrade. Each layer plays an important role for the durability and maintenance of the track geometry. The use of natural aggregates for constructing those layers represents a significant consumption of an important non-renewable resource that is becoming increasingly scarce. Using recycled materials in the construction and maintenance of railway track-bed can significantly reduce the consumption of natural resources and mitigate the need for the disposal of a solid waste.

In the last years, the growing popularity of recycled materials applied in road pavements and railway infrastructures, such as crumb rubber (CR) coming from end-of-life tires (ELTs), and reclaimed asphalt pavement (RAP) has sparked the conduction of several studies aiming at improving the materials circularity, in which the waste produced by some systems reduces the consumption of primary materials being needed by other ones as for instance the production of asphalt mixtures (Silva et al., 2012; Bressi et al., 2016a).

ELTs are among the largest and most problematic sources of waste due to the large volume produced and their durability (Lo Presti, 2013). On one hand, these characteristics are negative if ELTs are considered as waste material, but being very resistant and durable, CR obtained from the processing of ELTs has the potential to be an interesting material for use in other products, such as asphalt mixtures. Rubber grains are obtained from crushing scrap tires in specialized plants where they are also separated from steel fibers and textile. These grains can be incorporated into the preparation of asphalt mixtures by the so-called “wet” and “dry” production processes. The *wet process* envisages the dissolution of the CR in the bitumen as a modifying agent. The *dry process* envisages the replacement of a small portion of aggregates with the same fractions of rubber grains (FHWA 1997).

The use of CR in the production of asphalt mixtures by means of both technologies has proved to be environmentally beneficial due to: (i) the reduction of the Gross Energy Requirement (GER) and the greenhouse gas (GHG) emissions (Farina et al., 2016, Losa et al. 2012); (ii) the reduction of noise, especially when the dry process is used (Paje et al., 2010); and (iii) the improvement of damping properties when CR is mixed as an aggregate as a consequence of the vibrations absorption by the rubber (D’Andrea et al., 2004).

RAP is the milled material coming from the maintenance and rehabilitation (M&R) of asphalt pavements. The opportunity for using high amounts of RAP is underscored by the need of reducing the exploitation of quarries and the disposal of wastes resulting from road pavement construction and M&R. Often, these materials can be used to replace more costly virgin materials, provided that they ensure the same performance level as the traditional ones. This aspect seems not to be a practical limitation, given that several research works have proven that significant quantities of RAP can be

1 employed while keeping an acceptable level of performance (Santero et al., 2011; Yu and Lu, 2012;
2 Praticò et al., 2013; Bressi et al. 2016a). Moreover, the use of RAP materials to fully or partially
3 replace virgin and/or manufactured materials, thus avoiding their landfill or stockpile as waste, it is
4 also attractive for highway agencies to the extent that it reduces the cost of purchasing and
5 transporting new aggregate and binder for asphalt mixtures.

6 **2. Objective and Methodology**

7 The objective of this paper is to perform a comparative life-cycle assessment (LCA) of traditional
8 bituminous mixtures for sub-ballast, produced following the Italian standard specification of Rete
9 Ferroviarie Italiane (RFI), and bituminous sub-ballast mixtures containing different percentages of
10 recycled materials (i.e., RAP and CR).

11 In order to ascertain the extent to which the alternative sub-ballast mixtures allow achieving
12 environmental benefits when compared to the traditional sub-ballast mixtures, it is crucial to adopt a
13 life cycle approach able to identify and quantify the potential environmental burdens arising from the
14 use of these solutions. This need can be accomplished with the support of the LCA methodology
15 (ISO, 2006a) and the most recent standard on “Sustainability of Construction works” (EN 15804,
16 2012). LCA, which is a data-driven, systematic methodology, has proven to be effective in estimating
17 the environmental burdens caused by a product, process, or service throughout its life cycle
18 (Matthews et al., 2015). Among other capabilities, LCA assesses the potential impacts of the
19 emissions released to the environment as a consequence of the energy and materials consumed and
20 identifies opportunities for environmental improvements. The assessment includes the entire life
21 cycle of the product, process, or service and encompasses the extraction and processing of raw
22 materials, manufacturing, transportation, maintenance, use, and end-of-life (Consoli et al., 1993).
23 According to the ISO 14040 series the LCA framework is divided into four stages (ISO, 2006a; ISO,
24 2006b): (i) goal and scope definition; (ii) life cycle inventory analysis (LCI); (iii) life cycle impact
25 assessment (LCIA); and (iv) interpretation.

26 **2.1. Goal and scope definition**

27 *2.1.1. Goal*

28 The main goal of this research work is to quantify the potential life cycle environmental
29 impacts arising from the use of different types of alternative materials in the bituminous sub-ballast
30 layer, specifically CR obtained from processing ELTs and RAP coming from the demolition of old
31 road pavements. The results are compared with those associated with the use of traditional sub-ballast
32 mixtures. The findings of this study are intended to be used by engineering experts and practitioners
33 to make more assertive judgments on the advantages and disadvantages associated with the use of
34 emerging and commonly called sustainable strategies and practices for railway track-bed construction
35 and M&R.

36 The ReCiPe method (Goedkoop et al., 2013) was used to assess the potential environmental impacts.
37 This allowed covering several environmental interests because a list of LCI outputs are transformed
38 into values of indicators that are related to environmental impact categories. The analyses were
39 performed by using Gabi LCA software[®] and its database and processes. Specific processes not
40 available in Gabi (for instance CR production) were purposely created.

41

2.1.2. *System description and boundaries*

The system includes within its boundaries all the activities required to construct the bituminous sub-ballast layer. Specifically, the following phases are accounted for: (i) resources extraction and composite materials production; (ii) movement involved in hauling materials between facilities and work site; and (iii) construction equipment operation during the construction of the sub-ballast layer. The system boundaries tailored for the specific application carried out in this research work take into account the existing literature about the durability and performance of bituminous mixtures containing CR (dry process) and/or RAP. In this context, according to several recent studies (Farina et al., 2016; Lee et al., 2008; Fontes et al., 2010; Pinheiro and Soares, 2003; Gowda et al., 1996; Tam et al., 1992; McDaniel et al., 2000), CR dry and RAP mixtures can achieve the same performances of a traditional mixture, while few others instead report higher performance (Olivares et al., 2009; Airey et al., 2003; Sargious and Mushule, 1991; Huang et al., 2004). Therefore, a conservative approach assuming the same durability for all the solutions was considered. That means that the maintenance, dismantling and disposal phases are scheduled at the same time for all the solutions and then were excluded from the system boundaries.

The resources extraction and composite materials production consists of the acquisition and processing of raw materials, such as the bitumen production at refinery; extraction, crushing and sieving of aggregates, acquisition of crumb rubber generated as a by-product of the scrap tires crushing and sieving, and RAP processing.

The mixing process of asphalt mixtures takes place in hot mix production plants where bitumen is heated and pumped. Virgin aggregates are washed, dried, heated and added to the mixture, crumb rubber is added at room temperature while RAP is heated at lower temperature compared to the virgin aggregates. Indeed, it is important to heat the RAP as little as possible, as the heating ages the already aged binder further (Bressi et al., 2016b).

All the components are mixed in a batch-type mixing plant at the mixing temperature of 180°C. Afterwards, when the materials arrive at the construction site they are lay down with specific construction equipment and machinery, such as standard pavers and rollers. The transportation of materials to and from the construction site and between intermediate facilities are also considered.

2.1.3. *Functional unit*

The case study presented in this paper is referring to the railway track line between Florence and Viareggio in the Pistoia-Montecatini Terme section, Italy. The functional unit is a sub-ballast layer with a length of 1 km, a thickness of 12 cm and a width of 12.7 m. The thickness is equal for all the alternatives since it was assumed that all the solutions have the same durability.

2.1.4. *Asphalt mixtures types and composition*

Five types of bituminous mixtures for sub-ballast were considered in the application: the traditional mixture, complying with the RFI standard, and four mixtures with recycled materials, i.e., CR and RAP. In order to understand the potential environmental advantages and disadvantages related to the use of asphalt mixtures with recycled materials, mixtures with different percentages of RAP and CR were considered and compared with the reference scenario corresponding to the production and

1 placement of a classical bituminous sub-ballast mixture named RFI with 4% of bitumen by weight of
 2 mixture. The mixtures considered have the features described in the following:

- 3 • DRY1.5. Rubberized asphalt (dry process) containing 1.5% of CR and 5.5% of bitumen (both
 4 by weight of mixture).
- 5 • DRY2.0 Rubberized asphalt (dry process) containing 2.0% of CR and 6.0% of bitumen (both
 6 by weight of mixture).
- 7 • RAP30BR bituminous sub-ballast with 30% of RAP in partial substitution of virgin
 8 aggregates. This scenario considers that the bitumen trapped in RAP behaves as black rock
 9 (Shirodkar et al., 2010) not active in the new asphalt mixture. Black rock scenario
 10 corresponds to the 0% blending between RAP and virgin binder. Therefore, the percentage
 11 of the virgin bitumen to be added to the mixture cannot be reduced and has been kept equal
 12 to 4%.
- 13 • RAP30FB bituminous sub-ballast with 30% of RAP in partial substitution of virgin
 14 aggregates. This scenario considers 100% of aged bitumen trapped in the RAP being
 15 reactivated. The full blending between the RAP and virgin binder allows reducing the portion
 16 of virgin bitumen. Indeed, if RAP contains 5.5% of bitumen, it is necessary to add 3.3% of
 17 virgin bitumen in order to have a final content of 4% of total bitumen.

18 The composition of DRY1.5 and DRY2.0 results from a mix design optimization conducted in
 19 previous studies where it is shown also that higher amount of rubber can inhibit a satisfactory
 20 compaction in the laboratory due to the elastic behavior of the rubber (Bressi et al. 2017). For this
 21 reason, higher percentages of rubber were not considered.

22 Table 1 summarizes the composition of each bituminous mixture used as an alternative to the
 23 traditional bituminous sub-ballast (RFI) by showing the quantities of every element used to produce
 24 each alternative.

25

26 **Table 1. Composition of the different bituminous mixtures used in the sub-ballast layer.**

Type of mixture	Quantity of bitumen (kg per ton of mixture)	Quantity of aggregates (kg per ton of mixture)	Quantity of CR (kg per ton of mixture)	Quantity of RAP (kg per ton of mixture)
RFI mixture	40	960	-	-
DRY1.5 rubberized mixture with 1.5%	55	930	15	-
DRY2.0 rubberized mixture with 2.0%	60	920	20	-
RAP30BR with 30% of RAP by weight of aggregates and black rock (aged binder not reactivated)	40	672	-	288
RAP30FB with 30% of RAP by weight of aggregates and full blending (aged binder totally reactivated)	33	677	-	290

2.2. Life cycle inventory

The life cycle inventory (LCI) phase consists of the real data collection and modelling of the system. LCI data were collected from literature and interviews with designer, companies and experts involved in infrastructures construction works. The Ecopneus document (Ecopneus, 2013) was used as main reference for conducting the LCI of asphalt mixtures containing alternative materials. Reference values for the productivity and working hours of the machinery (pavers and rollers) considered for the laying down operations and compaction of the sub-ballast layers were collected from literature (Autostrade per l'Italia, 2011). For completing the data set and modelling the background system the *Construction materials database extension* of Gabi software was used.

2.2.1. Materials extraction and composite materials production phase

2.2.1.1. Virgin aggregates and bitumen production sub-phase

The virgin aggregates required for the sub-ballast were modelled as crushed gravel and the inventory data associated with their production were obtained from the *Construction materials database extension* of Gabi software. For modeling the production of sub-ballast material it is necessary to model the production of bitumen. The *Construction materials database extension* of Gabi software was also used as the data source for modelling the bitumen production. It comprises all the flows of materials and energy associated with the extraction, transport and refinement of crude oil.

2.2.1.2. Crumb rubber production sub-phase

Normally CR particles are obtained by reducing ELTs to small size grains (typically ranging from 4.75 mm to 0.075 mm) and removing the steel and textile from the scrap tires. One of the most common process to manufacture CR is the ambient grinding, i.e. a multi-step technology where tire chips are crushed in mills at ambient temperature (Shu and Huang, 2014). The chips are fed into a granulator that breaks them into small pieces. Afterwards, remaining steel is removed magnetically while for the fiber a combination of shaking screens and wind sifters are used.

In the *Construction materials database extension* of Gabi software, the process related to the production of CR is not available. Therefore, a new process *crumb rubber* was created by collecting information from a recent study conducted by Ecopneus (2013). A *Cut-off* approach was adopted for the evaluation of the burdens and benefits associated to the use of the recycled material. According to the *Cut-off* approach specified by the General Guide for Life Cycle Assessment (European Commission, 2010), only the burdens directly associated with the product itself are accounted for. Therefore, for the recycled materials derived from the ELTs the environmental impacts of the following processes were taken into account: (i) transport of materials from the collection platform to the recycling plant (crushing plant); (ii) the recycling process, including crushing and separation of the fibers and metal from the rubber; (iii) the sieving of different fractions; and (iv) the transport from the recycling plant to the hot mix asphalt plant. For the creation of the *crumb rubber production* process, it was necessary to build other two sub-processes: *Plastic big-bag production* to collect the CR grains after sieving (Figure 1a) and *Steel blade* to crush the scrap tires conveyed in the batch through a conveyor belt. (Figure 1b).



(a)



(b)

Figure 1. a) Mill and big bag to collect the rubber fractions and b) crushing process at the plant.

It was assumed that the *Plastic big-bag* used for collecting the different fractions of rubber grains are composed of 90% of polypropylene and 10% of polyethylene. The process contains all the operations and burdens for the transformation of raw plastic into the final product. The LCI of the plastic big bag production was collected from recent studies (Ruban, 2012; Pistonesi, 2017) and summarized in Table 2.

Table 2. Inventory referring to the production of 1 kg of Plastic big-bag.

Input Item	Quantity	Unit
Diesel [Refinery products] ^a	6,81E-05	kg
Polyethylene foam [Plastics] ^b	1	kg
Polyethylene low density granulate (LDPE/PE-LD) [Plastics] ^b	0,1	kg
Polypropylene granulate (PP) [Plastics] ^b	0,9	kg
Emissions to air and water		Quantity
Butyl acetate [ecoinvent long-term to air] ^a	0,0097	kg
Carbon dioxide [Inorganic emissions to air] ^a	0,00041	kg
Carbon monoxide [Inorganic emissions to air] ^a	8,06E-06	kg
Ethanol [ecoinvent long-term to air] ^a	0,00194	kg
Methane [Organic emissions to fresh water] ^a	3,26E-08	kg
Nitrogen dioxide [Inorganic emissions to air] ^a	4,10E-06	kg
Sulphur oxides [Inorganic emissions to air] ^a	5,00E-07	kg
Toluene [ecoinvent long-term to air] ^a	0,00399	kg

Notes: ^aRuban (2012); ^bPistonesi (2016).

The data for the modules *Polyethylene foam [Plastics]*, *Polyethylene low density granulate (LDPE/PE-LD) [Plastics]* and *Polypropylene granulate (PP) [Plastics]* include the production of the raw material. Thus all the processes from the resource extraction, acquisition and processing of raw materials were taken into account. Emissions to water and air are not tracked by the original modules, and then were gathered from a study conducted by Ruban (2012).

For the *steel blade* the processes selected are as follows: (i) steel production; (ii) hot rolling; and (iii) sheet rolling. The data set represents the steel production based on the main production steps, which take place within an integrated steel plant. The LCI of *steel blade* was collected from recent studies (Farina et al., 2016; Pistonesi, 2017) and it is covered by the processes *IT: electricity mix [supply*

1 *mix*] (0.00103 MJ), *Steel, converter, unalloyed, at plant, Sheet rolling, steel [processing]* present in
 2 Construction materials database extension of Gabi software.

3 These processes include the production of unalloyed steel, the transportation of the hot steel and other
 4 materials to the converter and the operation for pouring the melted steel into the mould. All the
 5 operations for heating, rolling and transforming the steel in a metallic sheet were also considered.

6 Once the processes *Steel blade* and *Plastic Big-Bag* production were created, they were included in
 7 the *crumb rubber* process. The input/output flows of materials and energy sources were calculated as
 8 the average value of the data collected from the Italian crushing plants.

9 The *crumb rubber production* is a multi-output process. Indeed, from the scrap tires treatment in
 10 specialized plants three main elements can be obtained: (i) CR (that will be used in the asphalt
 11 mixture); (ii) scrap steel; and (iii) textile. Therefore, the allocation of all the outputs was conducted
 12 according to the mass approach by using the following percentages: CR 69%, scrap steel output 20%
 13 and textile output 11% (Farina et al., 2016). Despite the high market value of steel, steel scrap was
 14 not assumed to undergo recycling for the high operational complexity of separating the scrap steel
 15 from residual rubber. Table 3 summarizes the input and output flows of the *crumb rubber production*
 16 process for producing 15 kg of rubber (1.5% of 1 ton of bituminous mixture).

17

18 **Table 3. Input and output flows associated with the *crumb rubber* process.**

Input flow	Quantity	Unit
Plastic big bag	0.028	Kg
Diesel mix at refinery EU-28 ^a	0.038	Kg
IT: Electricity mix grid production ^b	20.7	MJ
Lubricating oil	0.001	Kg
Tap water, at user	3.3	Kg
Steel blade	0.004	Kg
Conveyor belt, at plant	9.5E-005	m
Scrap tires	21.8	Kg
Output flows	Quantity	Unit
CR (module created)	15	Kg
Recycled fibers	2.4	Kg
Steel scrap product	4.35	Kg

19 Notes: ^a This module includes the steam treatment and allows quantifying all the output of the diesel
 20 production; ^b It refers to the production and importation of energy in Italy, including all types of
 21 energy. It includes also losses, calculated as average values.

22

23 **2.2.1.3. RAP production sub-phase**

24 Also for RAP production the *cut-off* approach was adopted. In this case study, it was considered that
 25 once removed from road pavement, the RAP is transported directly to the hot mix asphalt plant where
 26 it is stored in special sites and subjected to screening and down-sizing operations. For the RAP
 27 handling, the common production rates of the several machines integrating the processing unit were
 28 considered when determining the energy requirements. The LCI data related to the production and
 29 distribution of those energy resources were taken from the *Construction materials database extension*

1 of Gabi software. Moreover, the treatment of the RAP at the plant requires a certain amount of energy
2 for sieving and eventually crushing the recycled material. This amount of energy was considered to
3 be equal to 0.0212 MJ per kg of RAP (Zaumanis et al., 2012).

4 2.2.1.4. Asphalt mixtures production sub-phase

5 The mixture production activities take place in the hot mix production plant. The processes *crumb*
6 *rubber production*, *aggregates production*, *RAP production* and *bitumen production* already
7 described were created and fed into the process for the production of bituminous sub-ballast mixtures.

8 The electricity for the production of 1 ton of sub-ballast mixture was equal to 160 kWh (Ecopneus,
9 2013) and it was assumed to be the same for all the solutions because the fabrication temperature is
10 considered to be the same (Farina et al., 2016). In this case study the electricity is used to power a
11 discontinuous batch with a gas burner with a power of 580 kW.

12 2.2.2. Construction phase

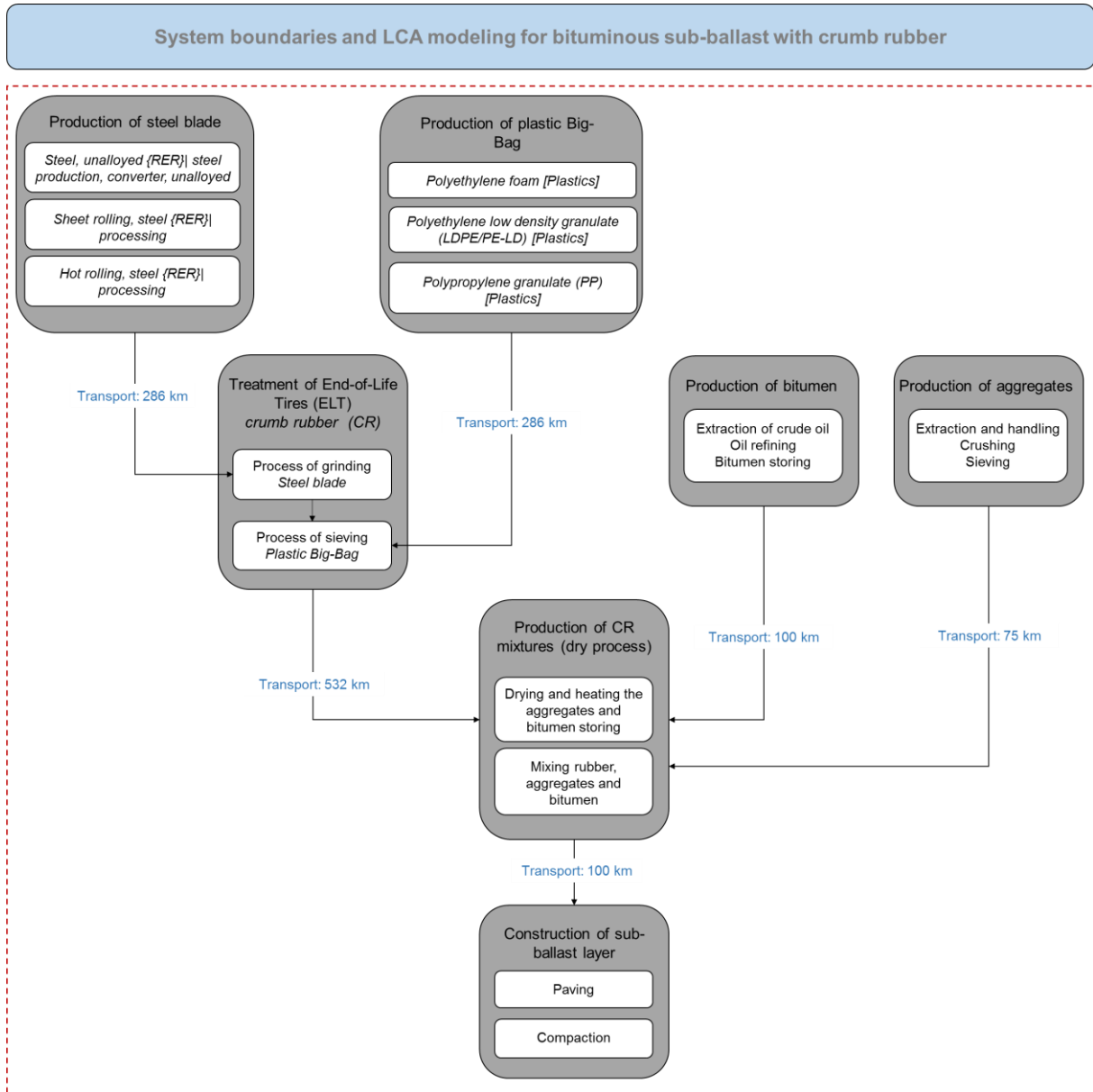
13 To build a layer of bituminous sub-ballast in a railway track it is necessary to lay down the bituminous
14 mixture with a paver and compact it in order to achieve the desired thickness of 12 cm. The fuel
15 combustion-related emissions associated with the operation of each construction equipment were
16 determined by combining the LCI data corresponding to the process “*machine operation, diesel, >=*
17 *74.57 kW, high load factor | machine operation, diesel, >= 74.57 kW, high load factor*” existing in
18 the *Construction materials database extension* of Gabi software with an hourly productivity of 150
19 t/h for the operations involved in pavement construction activities. By considering respectively fuel
20 consumption rates of 0.21 and 0.12 l/h (Autostrade per l’Italia, 2011) for a paver and a roller, their
21 fuel consumption rates were expressed in ton of material laid down and compacted. The consumptions
22 were considered to be the same for all the alternatives proposed. Indeed, even if recent studies (Bressi
23 et al. 2017) demonstrated the higher need of compaction of dry mixtures in the laboratory, there is no
24 practical link between laboratory increased compaction efforts and in-situ compaction in terms of
25 greater number of roller passages.

26 The airborne emissions caused by the lay down and compaction operations of bituminous layers
27 increases with recycling rate. Therefore, the data coming from measurements performed by Jullien et
28 al. (2006) were integrated in the process of sub-ballast installation depending on whether or not the
29 RAP is included in the mixture formulation.

30 2.2.3. Transportation of materials phase

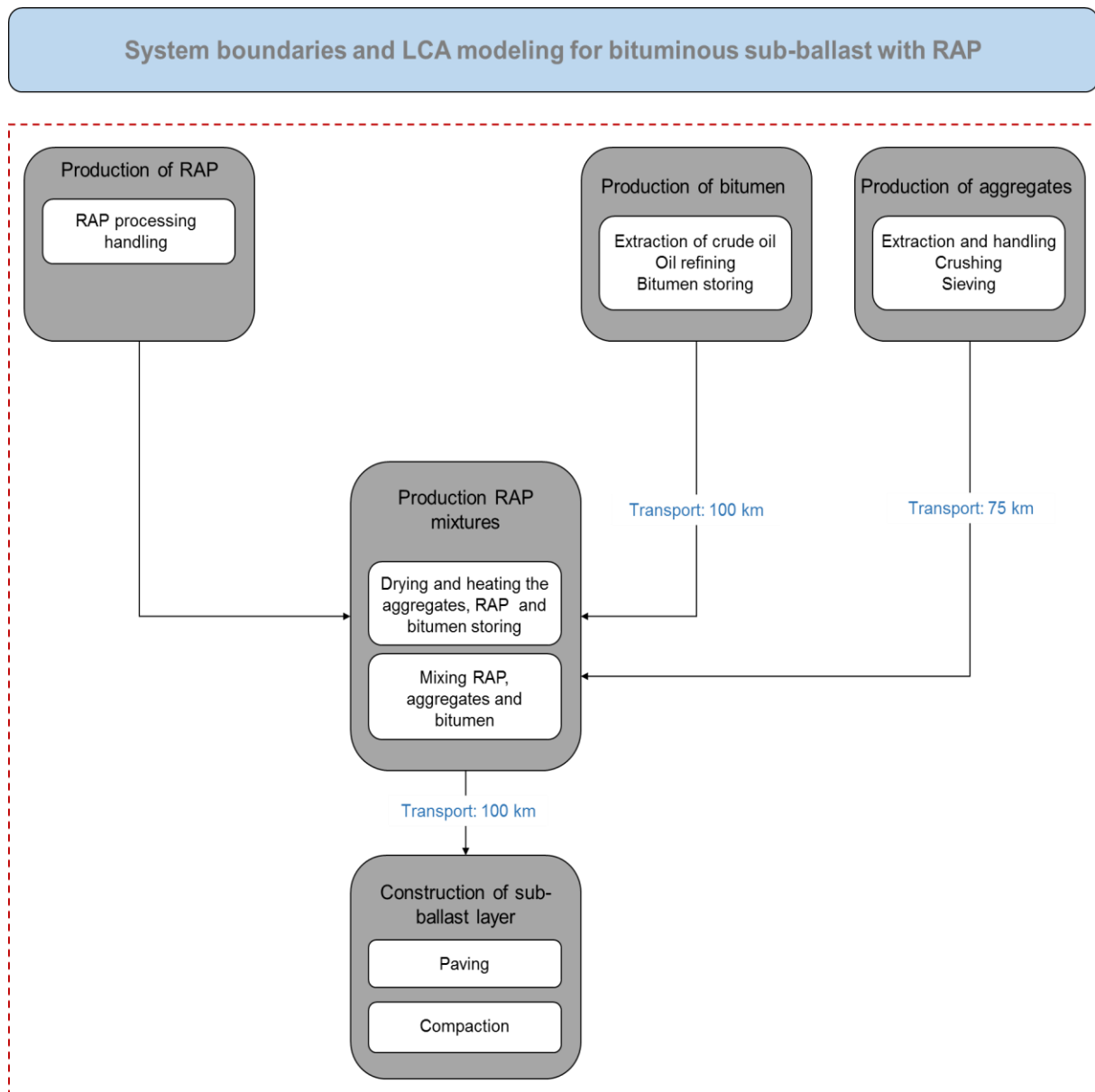
31 The crushed gravel limestone, bitumen as well as plastic big bag, steel blade and subsequently crumb
32 rubber must be transported between the production facilities, whereas the asphalt mixtures must be
33 transported from the hot mix production plant to the construction site. It was assumed that the
34 materials were hauled from the quarry and plants by truck. Therefore, the environmental impacts
35 resulting from the transportation of materials are due to the emissions released by the combustion
36 process of the transportation vehicles. All materials were assumed to be hauled by heavy duty
37 vehicles, and the process “*GLO: Truck, Euro 3, 20 - 26t gross weight / 17.3 t payload capacity ts <u-*
38 *so>*” existing in the *Construction materials database extension* of Gabi software was used to
39 determine the environmental burdens associated with the transportation of materials on the road.

1 The different processes adopted for the case study and the transport distances between the different
 2 sites are outlined in Figure 2 for the dry mixtures and Figure 3 for the RAP mixtures.



3
 4 **Figure 2. Schematic representation of the processes and transportation distances adopted for the**
 5 **bituminous sub-ballast layer with CR.**

6



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Figure 3. Schematic representation of the processes and transportation distances adopted for the bituminous sub-ballast layer with RAP.

4

2.3. Life cycle impact assessment

5

The life cycle impact assessment (LCIA) stage of the standardized LCA methodology comprises several steps, namely, classification, characterization, normalization, group and weighting (ISO, 2006a). Among these steps, classification and characterization were undertaken in this study.

6

7

8

The LCA was modeled in Gabi Professional Academy LCA software® (GaBi ts Software 7.3.3). The calculation of the impact category indicator results was performed at midpoint level by applying the impact assessment method ReCiPe (Goedkoop et al., 2013). Specifically, the following impact categories were considered: climate change, fossil depletion, freshwater ecotoxicity, freshwater eutrophication, human toxicity, marine ecotoxicity, marine eutrophication, metal depletion, ozone layer depletion, particulate matter formation, terrestrial acidification, terrestrial ecotoxicity and water depletion.

9

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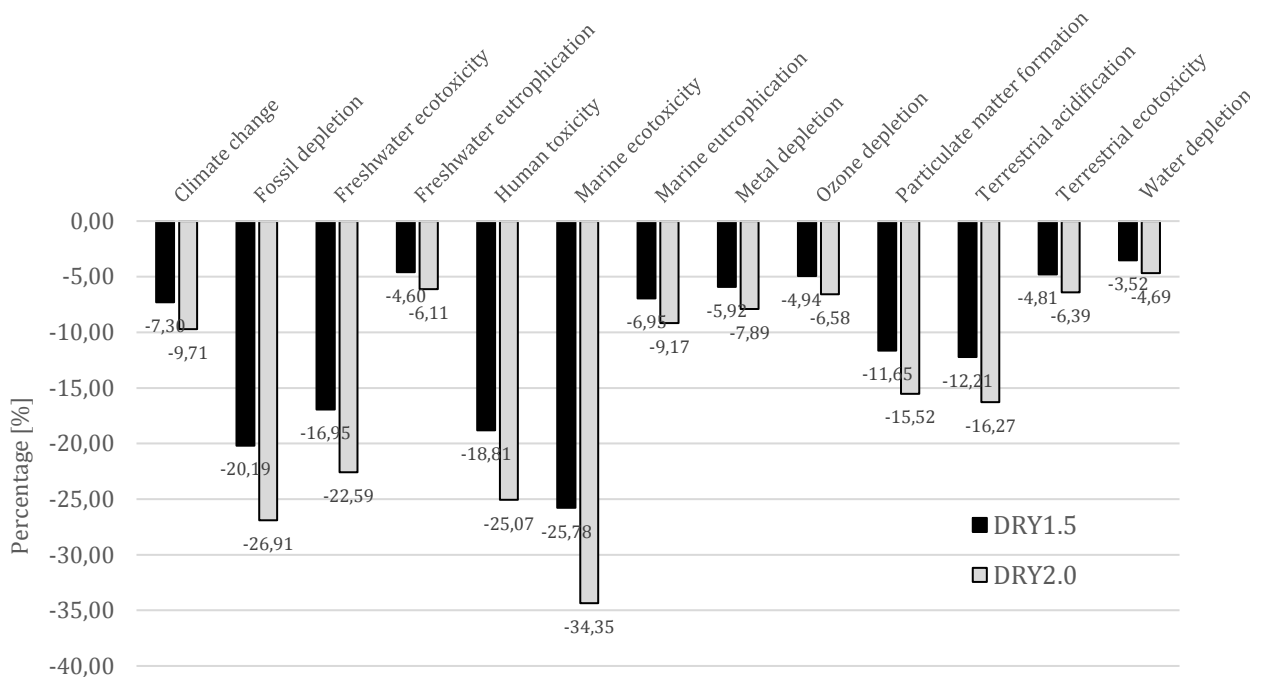
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1 **3. Results and discussion**

2 The LCA results shown in Figure 4 highlight different aspects of the environmental performance
 3 associated with each alternative proposed for the construction of the sub-ballast layer. In particular it
 4 displays the potential relative life cycle environmental impacts of the bituminous sub-ballast mixture
 5 containing CR (DRY 1.5 and DRY 2.0) for all impact categories, calculated in relation to those of the
 6 traditional bituminous sub-ballast mixture complying with RFI standard. The results are to be
 7 understood as follows: negative relative numbers mean that the alternative bituminous sub-ballast
 8 mixtures worsen the LCIA results in relation to those associated with the traditional bituminous sub-
 9 ballast mixture while positive numbers represent an improvement of the environmental profile.



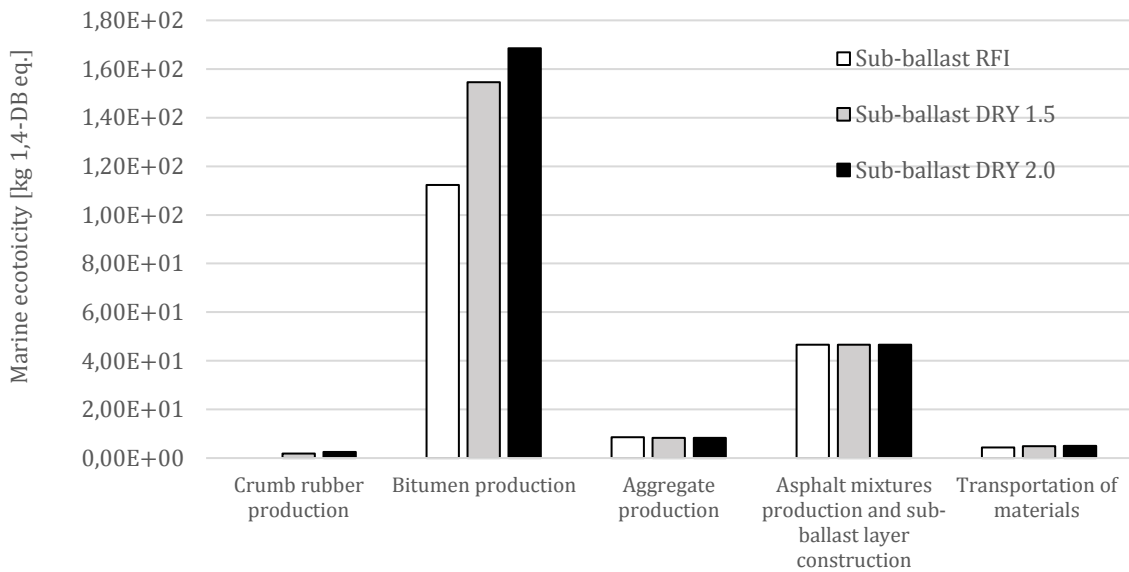
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11 **Figure 4. Potential relative life cycle environmental impacts of alternative bituminous sub-ballast**
 12 **mixtures (DRY 1.5 and DRY 2.0) calculated in relation to those of the base solution, i.e. the traditional**
 13 **bituminous sub-ballast mixture (RFI).**

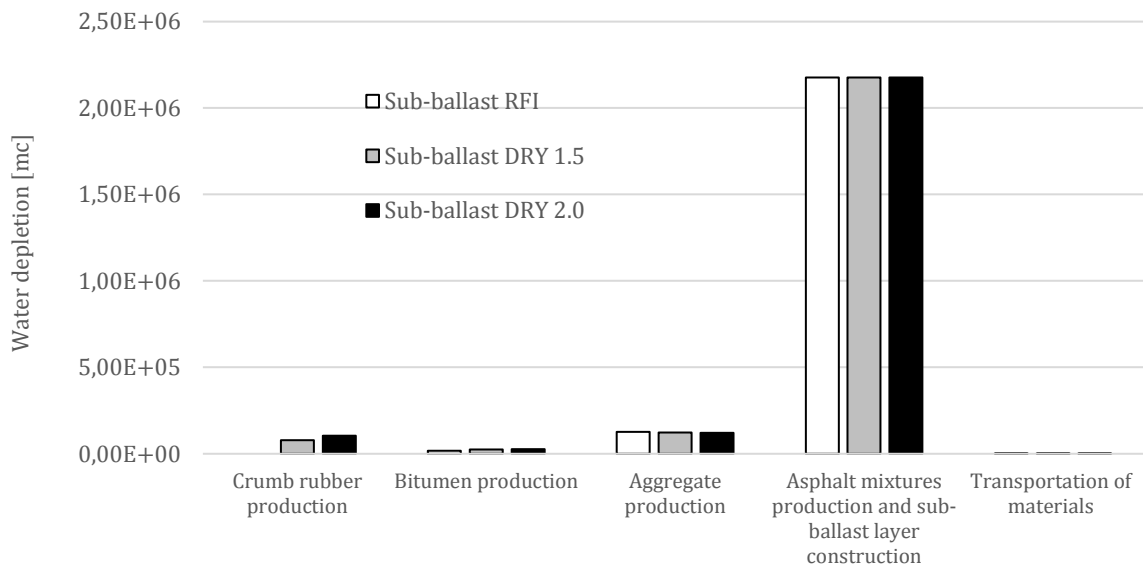
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15 As it can be seen from Figure 4 the use of bituminous sub-ballast mixtures containing crumb rubber
 16 leads to negative relative impacts in all categories, particularly in the case of the impact categories
 17 marine ecotoxicity (-34.35% for DRY2.0 and -25.78% for DRY1.5), fossil depletion (-26.91% for
 18 DRY2.0 and -20.19% for DRY1.5), human toxicity (-25.07 for DRY2.0 and 18.81% for DRY1.5)
 19 and freshwater ecotoxicity (-22.59% for DRY2.0 and -16.95% for DRY1.5). Moreover, the
 20 deterioration of the environmental profile is more pronounced when the quantity of rubber added to
 21 the mixture increases. These results can be explained by the following facts: i) the dry technology
 22 requires additional processes of crushing and treatment of the rubber in specialized plants where it is
 23 also separated from steel fibres and textile; ii) since rubber absorbs bitumen, the optimal binder
 24 content for CR mixtures is higher (i.e., 5.5 and 6% for 1.5 and 2% of CR respectively) than that for
 25 the traditional bituminous sub-ballast mixture (4%); iii) the amount of recycled materials that
 26 substitutes raw materials (i.e. virgin aggregates) is relatively low (1.5 or 2% by weight of the mixture).

1 Figure 5 shows the contributions given by the different sub-phases for the results observed in the
 2 impact categories marine ecotoxicity (Figure 5a), that presents the greatest deterioration, and water
 3 depletion (Figure 5b), that presents the lowest deterioration.



(a)

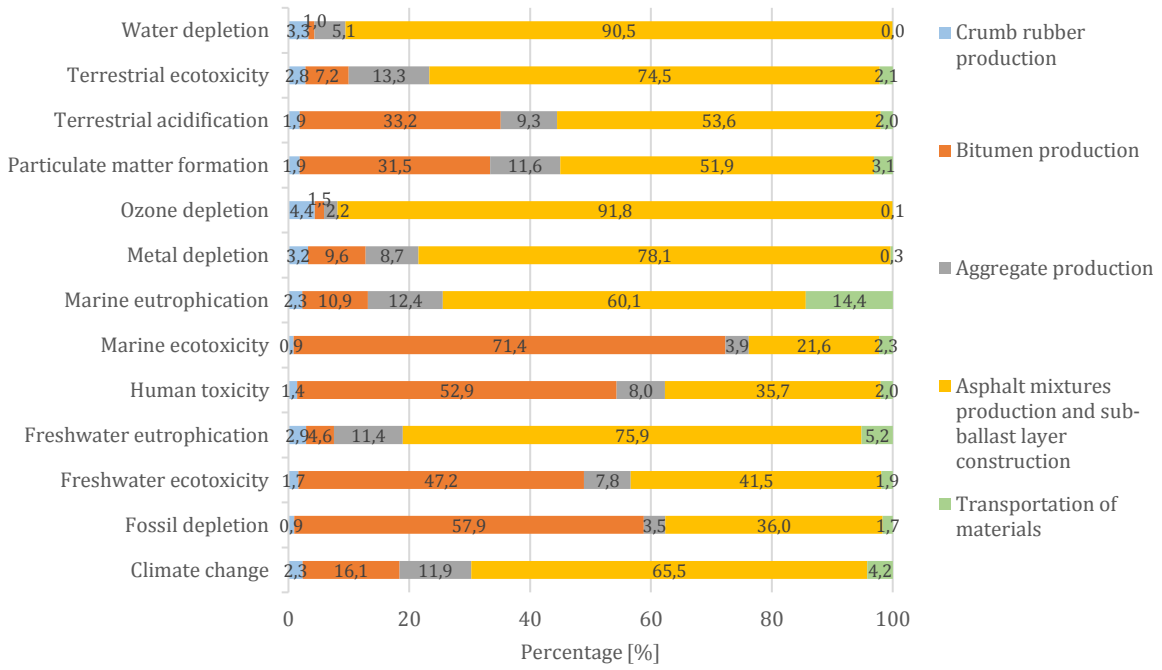


(b)

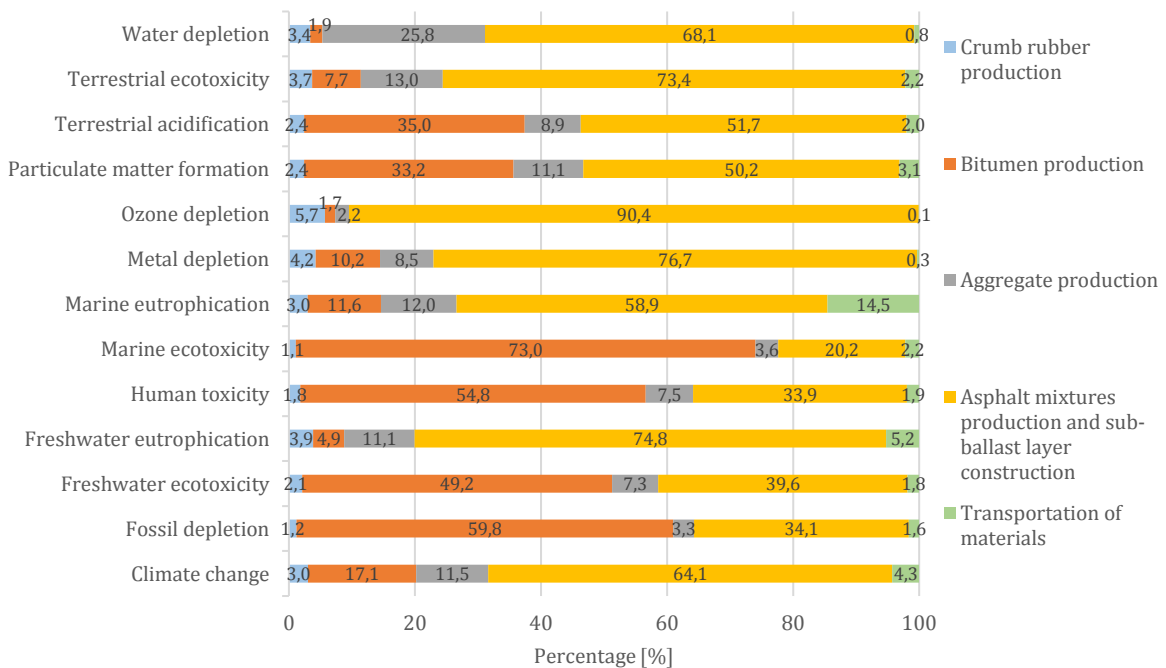
4 **Figure 5. Analysis of the contribution of different life cycle phases and sub-phases for the results**
 5 **observed in the a) marine ecotoxicity impact category and b) water depletion impact category for**
 6 **traditional sub-ballast mixture (RFI), sub-ballast DRY 1.5 and DRY 2.0 mixtures.**

7

8 Figure 5 confirms that the deterioration of the impact assessment results in the impact category marine
 9 ecotoxicity is essentially due to the increase of the optimal binder content for CR mixtures, which
 10 results in a higher impact in the bitumen production sub-phase, while the deterioration in the water
 11 depletion category is principally due to the additional processes of crushing and treatment of the
 12 rubber in specialized plants, which results in a higher impact in the crumb rubber production sub-
 13 phase.



(a)



(b)

1 **Figure 6. Relative contribution of different life cycle phases and sub-phases for the total environmental**
 2 **impacts due to the use of (a) bituminous sub-ballast mixture with 1.5% of CR and (b) bituminous sub-**
 3 **ballast mixture with 2.0% of CR.**

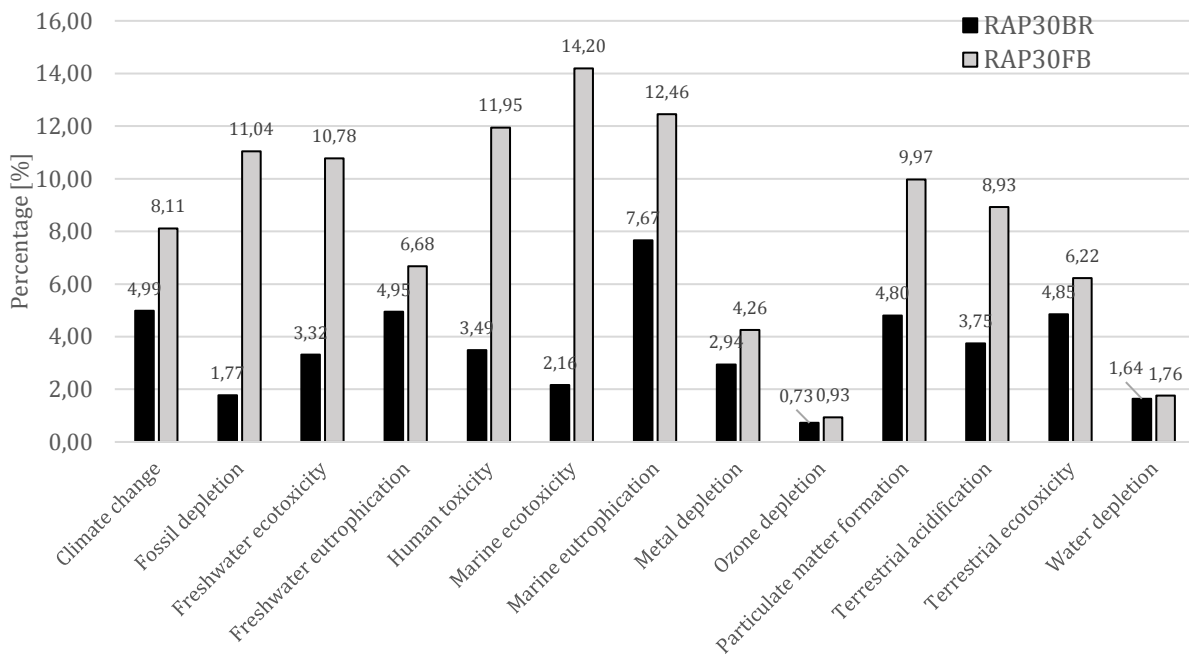
4

5 Figure 6 displays the relative contribution of the several life cycle phases and sub-phases to the total
 6 environmental impacts.

7 As detailed in Figure 6, the asphalt mixtures production and sub-ballast layer construction phases are
 8 the main source of impacts for 9 out of 13 impact categories, followed by the bitumen production (4
 9 out of 13 impact categories). In turn, the production of CR is responsible by the lowest share of the

1 impact scores. In the case of the asphalt mixtures production and sub-ballast layer construction their
 2 contribution can be as high as 91.8% and 90.4% for the impact category ozone depletion, respectively
 3 in the solutions DRY1.5 and DRY2.0, while the maximum contribution given by the production of
 4 bitumen can amount to 71.4% and 73.0% for the impact category marine ecotoxicity respectively in
 5 the solutions DRY1.5 and DRY2.0. Regarding the production of CR, its maximum contribution is
 6 observed for the impact category ozone depletion, being equal to 4.4% and 5.7%, respectively in the
 7 DRY1.5 and DRY2.0 solutions.

8 Figure 7 shows the potential relative life cycle environmental impacts of the bituminous sub-ballast
 9 mixtures containing RAP (RAP30BR and RAP30FB) in relation to those of the traditional bituminous
 10 sub-ballast mixture.



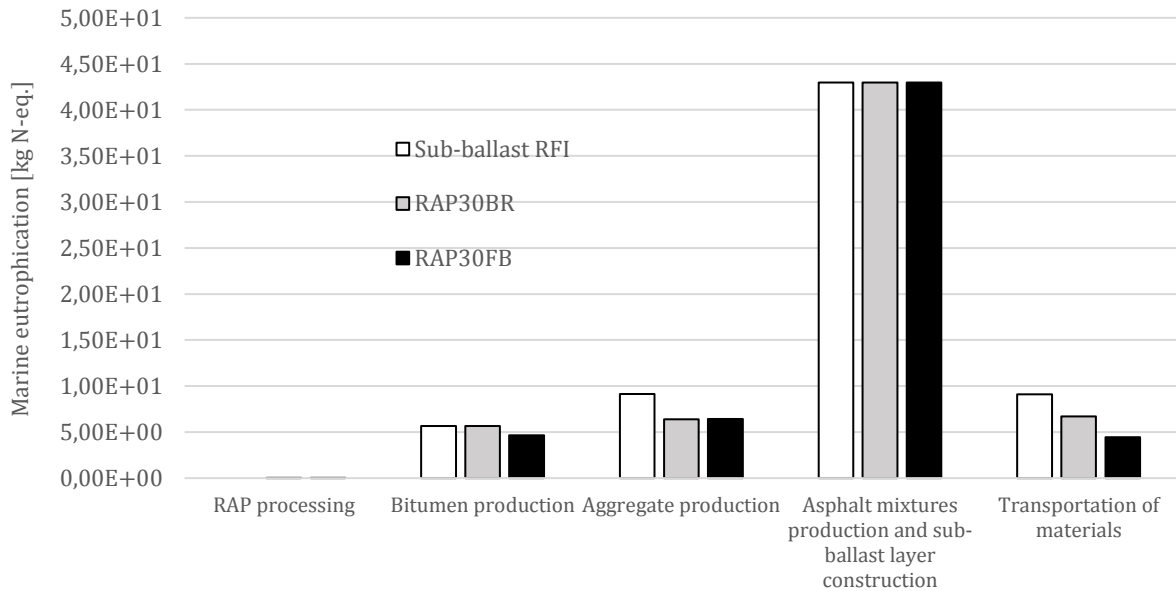
11

12 **Figure 7. Potential relative life cycle environmental impacts results of alternative bituminous sub-**
 13 **ballast mixtures (RAP30BR and RAP30FB) calculated in relation to those of the base solution, i.e. the**
 14 **traditional bituminous sub-ballast mixture (RFI).**

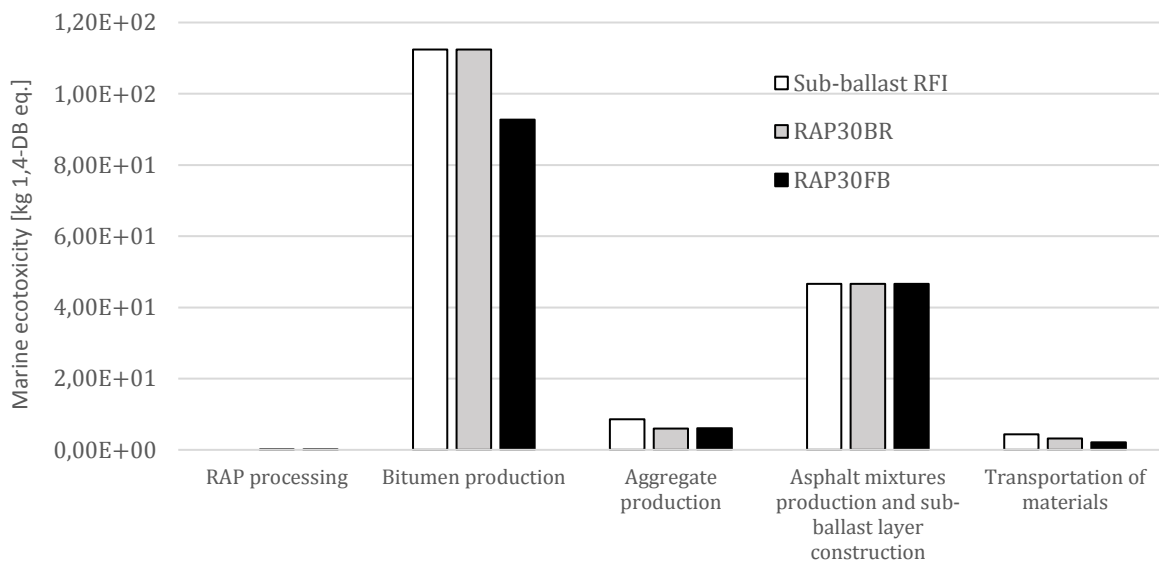
15 The solutions containing RAP reduce the environmental impacts compared to the reference solution
 16 in all the impact categories. In particular for the solution RAP30BR, which requires a lower quantity
 17 of virgin aggregates and the same content of bitumen as that of the reference mixture, the impact
 18 categories marine eutrophication (7.67%), climate change (4.99%), freshwater eutrophication
 19 (4.95%), terrestrial ecotoxicity (4.85%) and particulate matter formation (4.80%) show the higher
 20 benefits. It should be noted that when considering the full blending between the aged and virgin binder
 21 and reducing the quantity of virgin bitumen to be added to the mixture RAP30FB the impact
 22 categories exhibiting the higher benefits are different: marine ecotoxicity (14.20%), marine
 23 eutrophication (12.46%), human toxicity (11.95%), fossil depletion (11.04%) and freshwater
 24 ecotoxicity (10.78%). This means that the reduction of 30% of virgin aggregates has a greater effect
 25 on certain impact categories, while the bitumen reduction allows further reductions in all the impact
 26 categories, especially in the cases of the marine ecotoxicity, fossil depletion and human toxicity.

1 Figure 8 shows the contributions given by the different phases and sub-phases for the results observed
 2 in the impact categories marine eutrophication and marine ecotoxicity (Figure 8a, 8b), that present
 3 the greatest improvements respectively for the mixtures RAP30BR and RAP30FB, and ozone
 4 depletion (Figure 8c), that denotes the lowest improvement for both solutions.

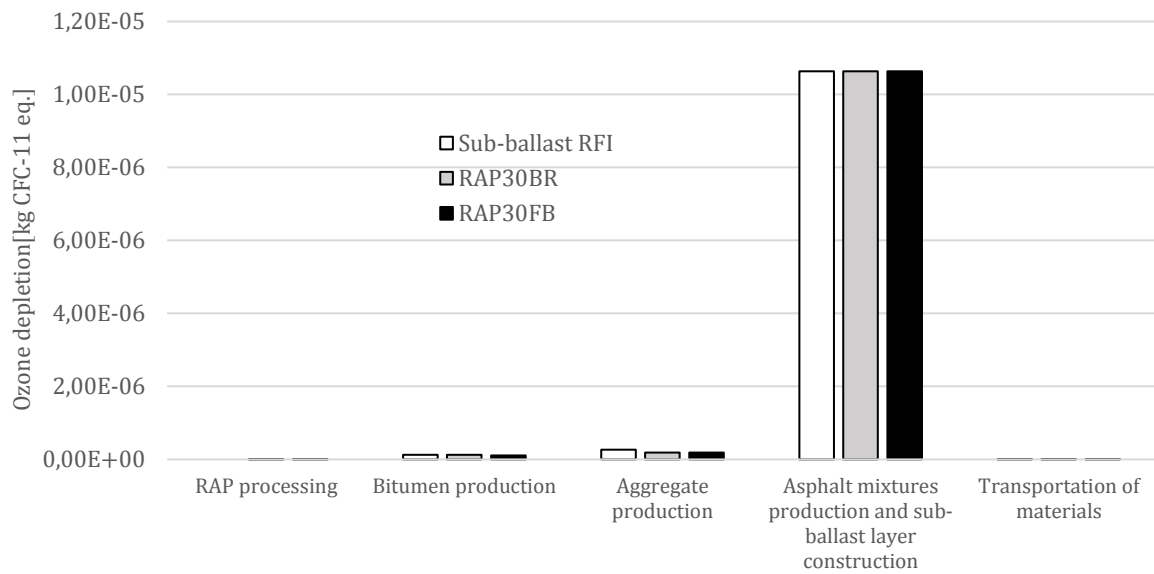
5



(a)



(b)



(c)

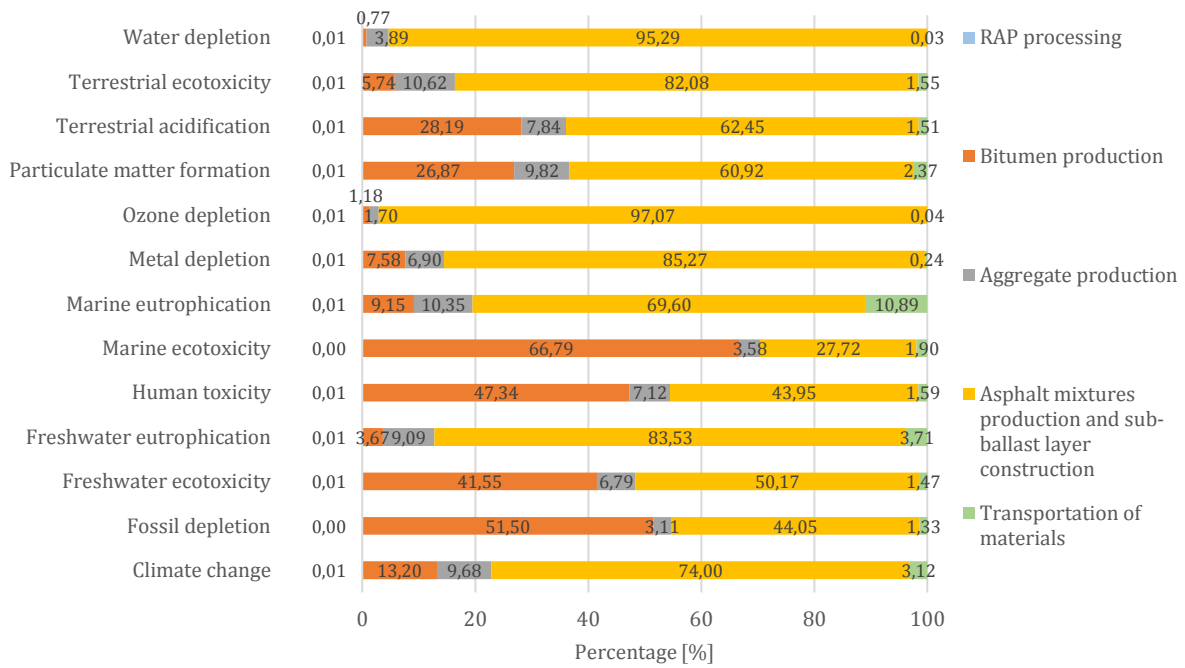
Figure 8. Analysis of the contribution of different life cycle phases and sub-phases for the results observed in the (a) marine eutrophication, (b) marine ecotoxicity and (c) ozone depletion for traditional sub-ballast mixture (RFI), sub-ballast RAP30BR mixture and sub-ballast RAP30FB mixture.

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4

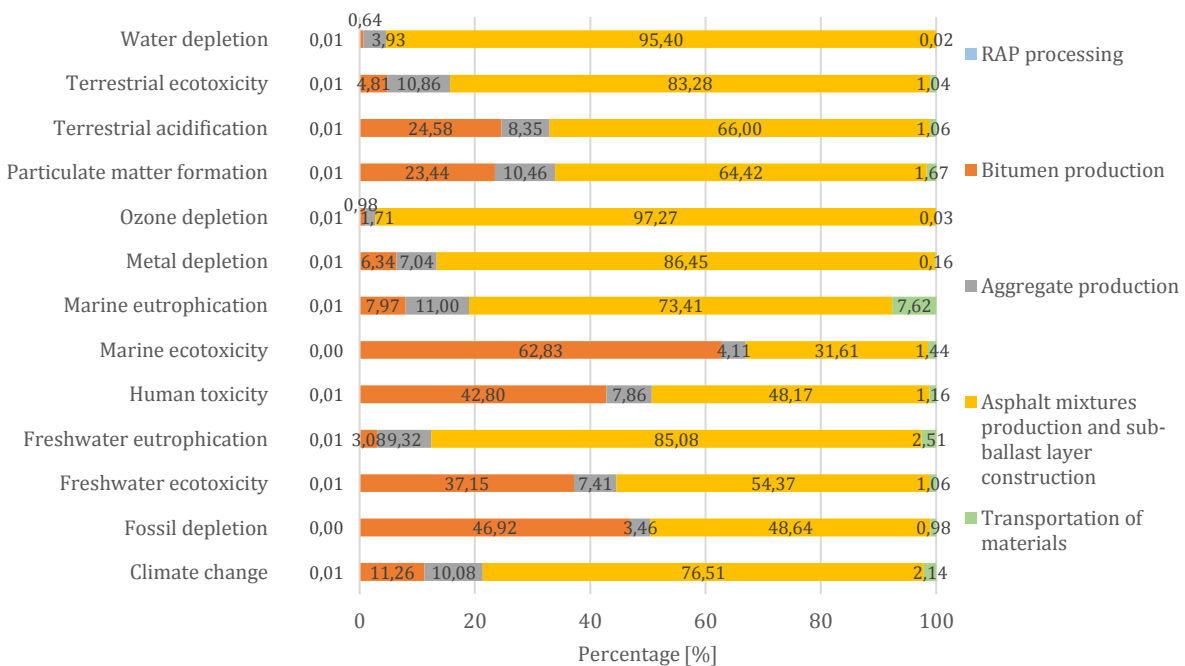
Figure 8 confirms that the environmental improvement observed in the impact category marine eutrophication is principally due to the reduction of the consumption of virgin aggregates, while the environmental improvement in the impact category marine ecotoxicity is due to the reduction of the consumption of virgin bitumen.

The production of virgin bitumen is one of the most environmental damaging and energy demanding processes, as confirmed by other recent studies (Santero et al., 2011; Santos et al., 2015; Farina et al., 2016). Therefore, the use of rejuvenators that can reactivate the aged binder is desirable, provided that the environmental impacts their production generate do not offset the benefits obtained with the reduction of the use of virgin bitumen. That seems to be the case of rejuvenators obtained from waste products, such as waste engine oil, waste engine oil bottoms, waste cooking/vegetable oil, vegetable grease, etc (Oreskovic et al., 2017).

Figure 9 shows the contribution of every phase and sub-phase to the total environmental impacts related to the construction of the sub-ballast layer when the asphalt mixtures employed contain RAP.



(a)



(b)

1 **Figure 9. Relative contribution of different life cycle phases and sub-phases for the total environmental**
 2 **impacts due to the use of (a) bituminous sub-ballast RAP30BR mixture and (b) bituminous sub-ballast**
 3 **RAP30FB mixture.**

4

5 As detailed in Figure 9, the asphalt mixtures production and sub-ballast layer construction phases are
 6 the main source of impacts for 11 out of 13 impact categories, followed by the bitumen production
 7 (2 out of 13 categories). In turn, the RAP processing is responsible by the lowest share of the impact
 8 scores (lower than 0.02% in all impact categories). In the case of the asphalt mixtures production and
 9 sub-ballast layer construction their contributions can be as high as 97.07% and 97.27% for the impact
 10 category ozone depletion, respectively in the RAP30BR and RAP30FB mixtures, while the maximum

1 contribution given by the production of bitumen can amount to 66.79% and 62.83% for the impact
2 category marine ecotoxicity respectively in the RAP30BR and RAP30FB mixtures. By observing
3 Figure 9 it can therefore be concluded that to reduce the total environmental impacts of sub-ballast
4 layer construction the attention should be focused on reducing the impacts related to bitumen and
5 asphalt mixtures production. The use of rejuvenators may reactivate the aged binder, thus allowing
6 the reduction of the use of virgin bitumen. Moreover, taking into account the weight denoted by the
7 production of asphalt mixtures for the environmental profile of the sub-ballast layer, it is then clear
8 that the adoption of solutions that allow a reduction in the production temperature such as warm and
9 cold mix asphalt techniques have the potential to originate substantial savings in terms of
10 environmental impacts. Indeed, the energy consumption and emissions released to the environment
11 are strongly related to the fabrication temperature during the mixing phase (Zaumanis et al., 2012).

12 **4. Summary, conclusions and perspectives**

13 Several research efforts are currently being undertaken to study the behavior of innovative mixtures,
14 in which a high content of recycled materials is used in their production. Nevertheless, the extent to
15 which those mixtures are environmentally sustainable remains to be assessed and quantified.
16 Therefore, this paper presents a comparative LCA of a traditional bituminous mixture to be employed
17 in the sub-ballast layer and alternative bituminous mixtures containing different percentages of
18 recycled materials, namely RAP and CR.

19 Asphalt mixtures design is nowadays tailored to obtain mixtures incorporating high-content of
20 alternative materials without under-performance. For this reason and without any clear evidence from
21 the literature, in the analyses carried out, the durability of the different types of sub-ballast mixtures
22 was assumed to be equal. On this basis, a LCA was performed from the resource extraction and
23 composite materials production to the construction site, and including the transportation of materials
24 movements, in order to highlight the principal differences among all the alternatives studied.

25 The results obtained showed that:

- 26 a) re-using ELTs within dry rubberized asphalt for railways sub-ballast layer is not more
27 environmentally sustainable than using conventional asphalt mixtures. In fact:
- 28 • without a certain increase in durability, the use of CR in bituminous sub-ballast
29 mixtures (DRY1.5 and DRY 2.0) leads to an increase of the scores in all impact
30 categories. This is principally due to the fact that the rubber grains are obtained from
31 crushing scrap tires in specialized plants where they are also separated from steel fibers
32 and textile. All these operations are extra in relation to those required for producing
33 traditional mixtures while the associated burdens are not compensated by the amount
34 of recycled material employed (only 1.5 or 2% of CR).
 - 35 • due to the rubber elasticity the rubberized asphalt usually recovers deformation after
36 the compaction phase. Therefore, by using a standard re-use of CR in asphalt mixtures,
37 the percentage of rubber in CR mixtures cannot be increased significantly, thus the
38 small amount used for this application does not justify all the additional consumption
39 of resources and emissions associated with its treatment.
 - 40 • for CR mixtures, the amount of bitumen increases as the amount of rubber in the
41 mixture increases. That happens because rubber absorbs the lighter parts of the
42 bitumen in the so called process “maceration”.

- 1 • the production of bitumen at refinery is one of the most environmental damaging and
2 energy demanding process.
- 3 b) the re-use of RAP material is a very promising application to improve the environmental
4 sustainability of asphalt mixtures. In fact:
 - 5 • mixtures containing 30% of RAP led to a reduction of the environmental impacts in
6 all the impact categories.
 - 7 • when the aged binder is fully reactivated and it is considered working as the virgin
8 bitumen, it is possible to reduce the amount of virgin bitumen employed in a new
9 mixture. This allows further reductions of all the resources consumed and emissions
10 released.
 - 11 • it is recommended the development and the use of rejuvenators able to reactivate the
12 aged binder trapped in RAP, provided that the environmental impacts of their
13 production do not offset the benefits obtained with the reduction of the use of virgin
14 bitumen.
- 15 c) for all the alternatives studied the contribution given by the asphalt mixtures production phase
16 to the total impacts associated with the construction of the sub-ballast layer was found to be
17 the highest. Therefore, to reduce the global environmental impacts it originates it is important
18 to produce asphalt mixtures at lower temperatures, from which warm and cold mix asphalt
19 techniques are examples.

20 Finally, the work presented in this paper offers an overview on the environmental sustainability
21 assessment of different alternatives for bituminous sub-ballast mixtures containing different types
22 and amounts of recycled materials intended to partially replace the use of virgin aggregates. The
23 calculations performed were based on several context-sensitive hypothesis and thus cannot be
24 considered neither exhaustive nor generalized. This research work opens the way to extend the study
25 to other materials, evaluating for instance the possible benefits deriving from the use of rejuvenators
26 (industrial or natural) when high RAP contents are used. Moreover, the availability of data to be used
27 in the LCA of these type of materials is still very limited. Therefore, further research efforts should
28 be employed to produce a more complete and robust LCI that will certainly improve the overall
29 quality of the LCA.

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38 does not constitute a standard, specification, or regulation.

39 **Disclosure statement**

40 The authors declare that they have no conflict of interest.

41 **References**

- 1 Airey G.D., Rahman M. M., Collop A. C., 2003. Absorption of Bitumen Into Crumb Rubber
2 Using the Basket Drainage Method. *Int. J. Pavement. Eng.* 4: 105.
- 3 Autostrade per l'Italia, 2011. Sustainability report. Estimate of emissions and CO2 savings
4 derived from the adoption of in situ pavement recycling activities (in Italian).
- 5 Bressi S., Dumont A.G., Partl M., 2016a A new laboratory methodology for optimization of
6 mixture design of asphalt concrete containing reclaimed asphalt pavement material.
7 *Materials and Structures/Materiaux et Constructions* Volume 49, Issue 12.
- 8 Bressi S., Cavalli M.C., Partl M., Tebaldi G., Dumont A.G., Poulikakos L., 2016b Particle
9 clustering phenomena in hot asphalt mixtures with high content of reclaimed asphalt
10 pavements. *Construction and building materials*.
- 11 Bressi S., Colinas N., Di Mino G. 2017 Analytical approach for the mix design optimization of
12 bituminous mixtures with crumb rubber (under review).
- 13 Caltrans. Asphalt Rubber Usage Guide. s.l., 2006: State of California Department of
14 Transportation, Materials Engineering and Testing Services.
- 15 Chester, M.V., and Horvath A., 2009. Environmental assessment of passenger transportation
16 should include infrastructure and supply chains. *Environmental Research Letters* 4: 024008
17 (8pp), doi: 10.1088/1748-9326/4/2/024008.
- 18 Consoli, Frank, SETAC (Society), LCA "Code of Practice" Workshop 1993. Guidelines for life-
19 cycle assessment: a "code of practice", Ed. 1, Society of Environmental Toxicology and
20 Chemistry, (SETAC), Pensacola, FL.
- 21 Crockford W.W., 1995 Recycling crumb rubber modified asphalt pavements. s.l.: Texas
22 Transportation Institute. Report FHWA/TX-95/1333-1F, 1995.
- 23 D'Andrea A., Urbani L., Bonin G., 2004. Traffic Vibration Camping Whit Innovative Materials:
24 Development And Calibration Of a Simulation Model. 2th International S.I.I.V. Congress.
25 27-29 October. Florence, Italy.
- 26 Ecopneus 2013. Evaluation of the carbon footprint of the production of crumb rubber from end-
27 of-life tires. Ecopneus, Milano, Italia.
- 28 European Commission, 2010. General guide for Life Cycle Assessment – Detailed Guidance.
29 Joint Research Centre Institute for Environment and Sustainability
- 30 Farina A., Zanetti M., Santagata E., Blengini 2016. G. Life cycle assessment applied to
31 bituminous mixtures containing recycled materials: Crumb rubber and reclaimed asphalt
32 pavement. *Resources, Conservation and Recycling*
33 <http://dx.doi.org/10.1016/j.resconrec.2016.10.015>.
- 34 Feraldi R., Cashman S., Huff M., Raahauge L., 2013 A life cycle assessment case study of
35 ground rubber production from scrap tires. *Int J Life Cycle Assess* (2013) 18:613–625 DOI
36 10.1007/s11367-012-0514-8.
- 37 Fontes P.L., Glicerio T., Jorge C., Paulo A., 2010. Evaluating Permanent Deformation in
38 Asphalt Rubber Mixtures. *Constr. Build. Mater.* 24:1193.

- 1 FHWA, 1997 User guidelines for waste and by-product materials in pavement construction.
- 2 GaBi ts Software 7.3.3 & Databases 2017 Edition. Manual.
- 3 Goedkoop, M.J., Heijungs, R., Huijbregts, M., De Schryver, A., Struijs, J., Van Zelm, R., 2013.
4 ReCiPe 2008. A life cycle impact assessment method which comprises harmonised category
5 indicators at the midpoint and the endpoint level. First edition, Report I: Characterisation.
- 6 Gowda G. V., D. K. Hall, R. Elliot. 1996. Arkansas' Experience with Rubber Modified Mixes
7 Using Marshall and SHRP Level I Mix Design Methods. Transportation Research Board.
8 Washington D.C.
- 9 Heitzman M., 1992 Design and Construction of Asphalt Paving Materials with Crumb Rubber
10 Modifier. Transportation Research Record.
- 11 Hicks G, Cheng D, Teesdale T, 2010. Assessment of Warm Mix technologies for use with
12 Asphalt Rubber paving application. Tech-Report-103TM.
- 13 Huang, B., Zhang Z., and King W., 2004. "Fatigue Crack Characteristics of HMA Mixtures
14 Containing RAP," Proceedings, 5th International RILEM Conference on Cracking in
15 Pavements, Limoges, France.
- 16 Huang Y., Bird R., Heidrich O. 2007. A review of the use of recycled solid waste materials in
17 asphalt pavements. Resources, Conservation and Recycling 52 (2007) 58–73.
- 18 Hugo M.R.D. Silva, Joel R.M. Oliveira, Carlos M.G. Jesus., 2012. Are totally recycled hot mix
19 asphalts a sustainable alternative for road paving? Resources, Conservation and Recycling
20 60 38–48.
- 21 ISO 14040, 2006. Environmental Management - Life-cycle assessment - Principles and
22 framework. Geneva: International Organization for Standardization.
- 23 ISO 14044, 2006. Environmental management – Life cycle assessment – Requirements and
24 guidelines. Geneva: International Organization for Standardization.
- 25 Jones D, Wu R, Barros C, Peterson J., 2012. Research findings on the use of rubberized warm-
26 mix asphalt in California. Asphalt-Rubber 2012.
- 27 Jullien A., Moneron P., Quaranta G., Gaillard D., 2006. Air emissions from pavement layers
28 composed of varying rates of reclaimed asphalt. Resources, Conservation and Recycling 47
29 (2006) 356–374.
- 30 Lee S. L., Akisetty C. K., Amirkhanian S., 2008. The Effect of Crumb Rubber Modifier on the
31 Performance Properties of Rubberized Binders in HMA pavements. Constr Build Mater. 22:
32 1368.
- 33 Lo Presti D., 2013. Recycled Tyre Rubber Modified Bitumens for road asphalt mixtures: A
34 literature review. Construction and Building Materials.
- 35 Losa, M., Leandri, P., Cerchiai, M. Improvement of pavement sustainability by the use of crumb
36 rubber modified asphalt concrete for wearing courses (2012) International Journal of
37 Pavement Research and Technology, 5 (6), pp. 395-404.

- 1 Matthews, H., Hendrickson, C., Matthews, D., 2015. Life cycle assessment: quantitative
2 approaches for decisions that matter. Green Design Institute, Carnegie Mellon University,
3 Pittsburgh.
- 4 McDaniel, R. S., H. Soleymani, R. M. Anderson, P. Turner, and R. Peterson, 2000
5 Recommended Use of Reclaimed Asphalt Pavement in the SuperPave Mixture Design
6 Method, NCHRP Final Report (9-12), TRB, Washington, D.C.
- 7 Olivares F., Schultz B., Fernández M., Moro B., 2009. Rubber-modified Hot Mix Asphalt
8 Pavement by Dry Process. *Int. J. Pavement Eng.* 10:277.
- 9 Oliver JWH. 1981. Modification of paving asphalts by digestion with scrap rubber. [ed.]
10 Transportation Research Board. Transportation Research Record 821.
- 11 Oreskovic M., Bressi S., Di Mino G., Lo Presti D., 2017. Influence of bio-based additives on
12 RAP clustering and asphalt binder rheology. BCRRA Athens.
- 13 Paje, Bueno M., Terán F., Mirò R., Pérez-Jiménez F., Martínez A.H., 2010. Acoustic field
14 evaluation of asphalt mixtures with crumb rubber. Technical note. *Applied Acoustics*
- 15 Pinheiro J. H. M., Soares J. B., 2003. The Effect of Crumb Rubber Gradation and Binder-rubber
16 Interaction Time on the Asphalt-rubber mixture (Dry Process). Proc. of the Asphalt-Rubber
17 Conference. Brasilia, Brazil.
- 18 Pistonesi L. 2017 Valutazione della sostenibilità ambientale della sede ferroviaria in relazione a
19 diverse tipologie d sub-ballast. University of Pisa.
- 20 Praticò F.G., Vaiana, R., Giunta, M., 2013. Recycling PEMs back to TLPAs: Is that possible
21 notwithstanding RAP variability? *Applied Mechanics and Materials*, Volume 253-255, Issue
22 PART 1, Pages 376-384.
- 23 RFI capitolato costruzioni opere civili. sezione xv sub-ballast - pavimentazioni stradali.
- 24 Ruban, A., 2012: Life Cycle Assessment of Plastic Bag Production. Master thesis in Sustainable
25 Development at Uppsala University, 36 pp, 30 ECTS/hp.
- 26 Sacramento County. 1999. Report on the status of rubberized asphalt traffic noise reduction in
27 sacramento county. Sacramento County and Bollard & Brennan Inc.
- 28 Santero, N., Masanet, E., Horvath, A., 2011. Life cycle assessment of pavements. part I: critical
29 review. *Resour. Conserv. Recycl.* 55 (9–10), 801–809.
- 30 Santos, J., Ferreira, A., Flintsch, G., 2015. A life cycle assessment model for pavement
31 management: road pavement construction and management in Portugal. *Int. J. Pavement Eng.*,
32 16(4), 315-336.
- 33 Sargious, M., and Mushule N., 1991, “Behavior of Recycled Asphalt Pavement at Low
34 Temperatures,” *Canadian Journal of Civil Engineering*, Vol. 18, pp. 428-435.
- 35 Schwarz, H., 2009. Carbon Footprint of High-speed Railway Infrastructure (Pre-study).
36 International Union of Railways.

- 1 Shirodkar P., Y.A. Mehta, A. Nolan, K. Sonpal, A. Norton, C. Tomlinson, R. Sauber, E. DuBois,
2 2010. A study to determine the degree of partial blending of reclaimed asphalt pavement
3 (RAP) binder for high RAP hot mix asphalt, in: TRB 2010 Annual Meeting.
- 4 Shu X., Huang B., 2014. Recycling of waste tire rubber in asphalt and portland cement concrete:
5 An overview. Construction and Building Material.
- 6 Tam, K. K., Joseph P., and Lynch D.F. 1992. "Five-Year Experience of Low-Temperature
7 Performance of Recycled Hot Mix," Transportation Research Record, No. 1362,
8 Transportation Research Board, Washington, D.C., pp. 56-65.
- 9 Waste and Chemicals for Ecopneus, 2016. Esposizione dei lavoratori a inquinanti presenti in
10 miscele bituminose con addizione di polverino da PFU.
- 11 Yu B. and Lu Q., 2012 Life cycle assessment of pavement: methodology and case study.
12 Transportation and research part D 17 pp. 380-388.
- 13 Zaumanis M. et al., 2012. Calculation of asphalt production energy flow to compare warm and
14 hot mix asphalt. 5th Eurasphalt & Eurobitume Congress, 13-15th June 2012, Istanbul.